

# DUAL-BAND MICROWAVE HILBERT TRANSFORMER BASED SINGLE SIDE BAND MODULATION



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STATUS QUO

**Input** → **Hilbert Transformer**  $H(\omega) = -j \operatorname{sgn}(\omega)$  → **Output**

**Magnitude Response**

**Phase Response**

**Conventional Designs**

- ✓ Optical Regime
- ✓ Bulky and complex
- ✓ Costly fiber grating, nonplanar structures
- ✓ Inappropriate for spectrum aggregation.

Schematic of conventional HT

**NEW INSIGHTS**

**Dual-Band Microstrip line Hilbert Transformer**

- ✓ Suitable for Real-Time Analog Signal Processing.
- ✓ Unity magnitude and 180° Phase rotation at both design frequencies.
- ✓ Contains a dual-band 180° coupler and a dual-band delay line.
- ✓ Uses low-cost planar microstrip line technology.
- ✓ Capable of supporting Spectrum Aggregation.
- ✓ Edge detection and single side band modulation with Spectrum aggregation.

**Usage:** Edge Detection, Single Side Band Modulation, RADAR Communication, 3D Imaging etc.

DESCRIPTION

**Dual-Band 180° Coupler**

**Dual-Band 180° Coupler Design**

$$\begin{bmatrix} A & B \\ C & D \end{bmatrix}_{e/o} = \begin{bmatrix} 1 & 0 \\ Y_{in1} & 1 \end{bmatrix} \times \begin{bmatrix} \cos \theta & jZ \sin \theta \\ j \sin \theta & \cos \theta \end{bmatrix} \times \begin{bmatrix} 1 & 0 \\ Y_{in2} & 1 \end{bmatrix}$$

$$S_{34e/o} = \frac{A_{e/o} + B_{e/o}/Z_0 + C_{e/o}Z_0 + D_{e/o}}{2}$$

$$S_{34} = \frac{S_{34e} + S_{34o}}{2}$$

✓  $(\angle S_{34})$  at  $f_1$  and  $(\angle S_{34})$  at  $f_2$  are noted for the selected dual-band coupler.

Even-Odd Mode analysis

**Design of Dual-Band Delay Transmission Line**

**Design criteria**

- $|S_{xx}|_{f_1} = |S_{xx}|_{f_2} = 0$
- $|S_{xy}|_{f_1} = |S_{xy}|_{f_2} = 1$
- $(\angle S_{xy})_{f_1} = 2\pi - (\angle S_{34})_{f_1}$
- $(\angle S_{xy})_{f_2} = 4\pi - (\angle S_{34})_{f_2}$

✓ 4 design criteria, 6 unknowns ( $Z_p, Z_m, Z_s, \theta_p, \theta_m, \theta_s$ ).

✓ Assume  $Z$  values within 20 to 140Ω and solve for  $\theta$  values.

**ABCD Matrix**

$$\begin{bmatrix} A_r & B_r \\ C_r & D_r \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ jB_p & 1 \end{bmatrix} \times \begin{bmatrix} \cos \theta_m & jZ_m \sin \theta_m \\ j \sin \theta_m & \cos \theta_m \end{bmatrix} \times \begin{bmatrix} 1 & 0 \\ jB_s & 1 \end{bmatrix} \times \begin{bmatrix} \cos \theta_s & jZ_s \sin \theta_s \\ j \sin \theta_s & \cos \theta_s \end{bmatrix}$$

SIMULATED VS MEASURED RESPONSE OF HT

**Magnitude Response**

**Phase Response**

- ✓ Design frequencies 0.9 GHz and 1.98 GHz
- ✓ Passband bandwidths ~240MHz at both frequencies
- ✓ More than 10dB return losses.
- ✓ Passband Magnitudes ~-2dB except the presence of notches.
- ✓ 180° phase transition BW ~50MHz.

**Fabricated Hilbert Transformer**

APPLICATION IN DUAL-BAND SSB OPERATION

**Block Diagram of SSB Operation**

**Simulated vs Measured Response**

- ✓ Dual-band single side band operation with
  - passband of ~80MHz at both frequencies
- ✓ More than 10dB return losses.
- ✓ Passband Magnitudes ~-2dB

**Fabricated Dual-Band SSB Modulator**